

Chapter 4

Position (Displacement) Analysis

Why??

- Understand the displacement of a machine at any time (extreme positions may not be sufficient to understand the motion)
- Understand the dynamics of a machine

$$F = m \begin{matrix} a \\ \downarrow \\ \frac{dv}{dt} \\ \downarrow \\ \frac{dx}{dt} \end{matrix}$$

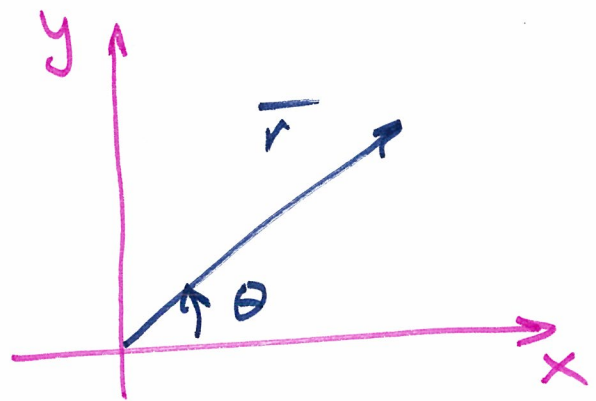
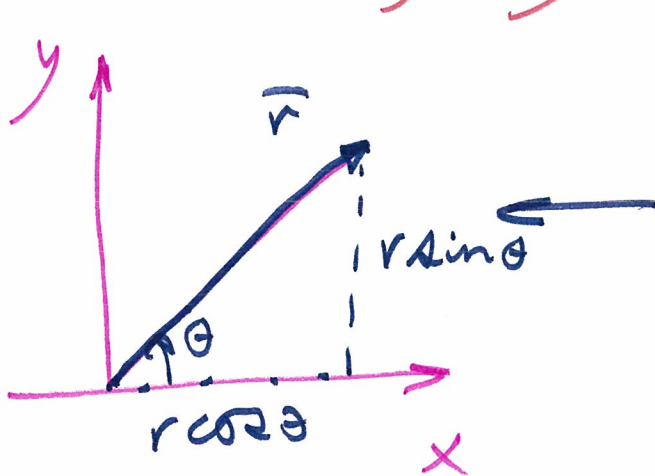
Background

$$j = \sqrt{-1}$$

$$e^{j\theta} = \cos \theta + j \sin \theta \rightarrow \text{De Moivre Theorem}$$

Alternative method for describing displacement (position) (2-D planar)

Let y-axis be associated with imaginary number j ($\sqrt{-1}$)



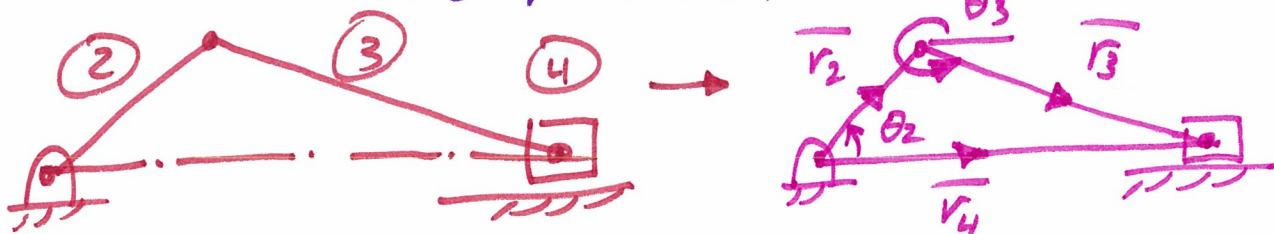
$$\bar{r} = r(\cos \theta + j \sin \theta)$$

magnitude $= r e^{j\theta}$

complex phasor

Advantage: combine x & y components

Example: Use complex phasors to analyze position of crank-slider mechanism



① Associate all links with vectors

② Create a vector loop equation

All angles should be measured CCW with respect to x-axis

$$\vec{r}_2 + \vec{r}_3 = \vec{r}_4 \longrightarrow \text{Alternative}$$

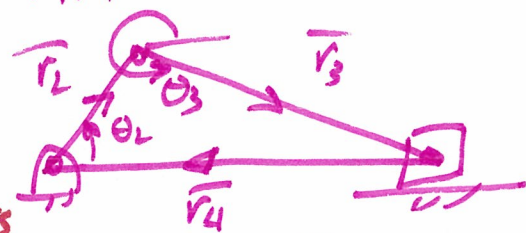
③ Write the vector loop equation in terms of complex phasors

$$r_2 e^{j\theta_2} + r_3 e^{j\theta_3} = r_4 e^{j\theta_4}$$

$$r_2 e^{j\theta_2} + r_3 e^{j\theta_3} = r_4$$

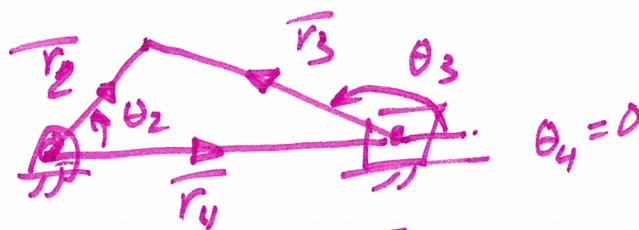
④ Identify input & outputs

input: θ_2
output: θ_3, r_4



$$\theta_4 = \pi \quad \vec{r}_2 + \vec{r}_3 + \vec{r}_4 = 0$$

OR



$$\vec{r}_2 = \vec{r}_4 + \vec{r}_3$$

All angles should be measured at the start of the vector

⑤ Replace $e^{j\theta}$ by $\cos\theta + j\sin\theta$

$$r_2(\cos\theta_2 + j\sin\theta_2) + r_3(\cos\theta_3 + j\sin\theta_3) = r_4$$

⑥ Separate into real and imaginary equations

$$\text{real} \rightarrow r_2 \cos\theta_2 + r_3 \cos\theta_3 = r_4 \quad (1)$$

$$\text{imag.} \rightarrow r_2 \sin\theta_2 + r_3 \sin\theta_3 = 0 \quad (2)$$

⑦ Solve for the outputs in terms of the inputs & fixed terms

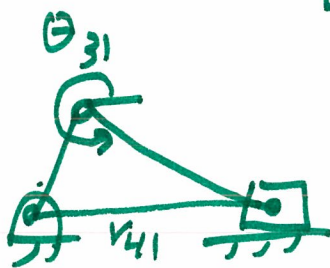
From (2)

$$r_3 \sin\theta_3 = -r_2 \sin\theta_2$$

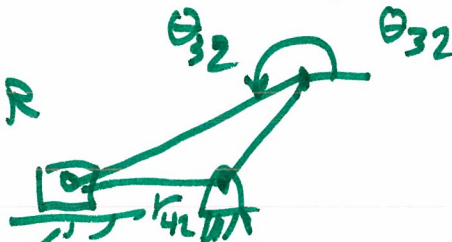
$$\sin\theta_3 = \frac{-r_2 \sin\theta_2}{r_3}$$

$$\theta_3 = \sin^{-1}\left(\frac{-r_2 \sin\theta_2}{r_3}\right)$$

↳ 2 values
↳ 2 closures: θ_{31} θ_{32}



OR



substitute in (1)

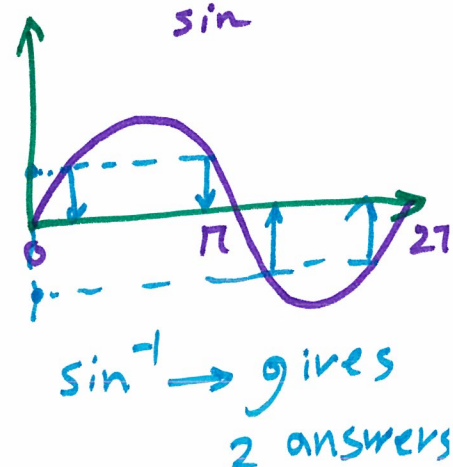
$$r_{41} = r_2 \cos\theta_2 + r_3 \cos\theta_{31}$$

$$r_{42} = r_2 \cos\theta_2 + r_3 \cos\theta_{32}$$

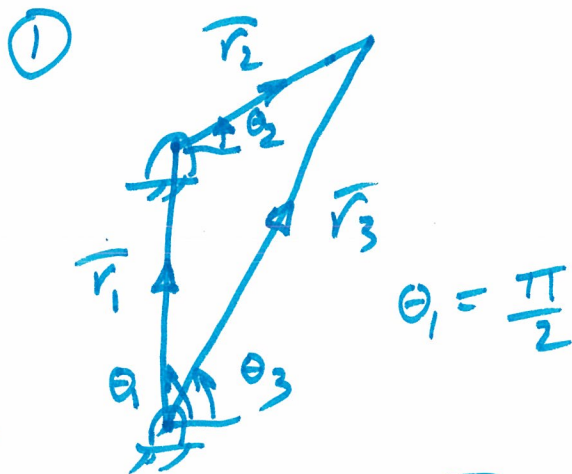
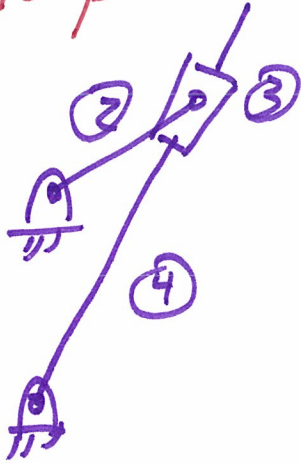
$$\left. \begin{aligned} a + jb &= 0 \\ \downarrow \\ a &= 0 \\ b &= 0 \end{aligned} \right\} \begin{array}{l} \text{solutions} \\ \text{coefficients} \end{array}$$

$$(a+c) + j(b+d) = 0$$

$$\left. \begin{aligned} a+c &= 0 \\ b+d &= 0 \end{aligned} \right\}$$



Example: Displacement Analysis of the first loop of the shaper QRM



② $\vec{r}_1 + \vec{r}_2 = \vec{r}_3$

③ $r_1 e^{j\theta_1} + r_2 e^{j\theta_2} = r_3 e^{j\theta_3}$

④ input: θ_2
output: θ_3 r_3

⑤
$$r_1 (\cos \theta_1 + j \sin \theta_1) + r_2 (\cos \theta_2 + j \sin \theta_2) = r_3 (\cos \theta_3 + j \sin \theta_3)$$

$$r_1 (\cos \frac{\pi}{2} + j \sin \frac{\pi}{2}) + r_2 (\cos \theta_2 + j \sin \theta_2) = r_3 (\cos \theta_3 + j \sin \theta_3)$$

$$r_1(0+j) + r_2(\cos\theta_2 + j\sin\theta_2) = r_3(\cos\theta_3 + j\sin\theta_3)$$

$$\begin{aligned} \text{⑥ real} &\rightarrow r_2 \cos\theta_2 = r_3 \cos\theta_3 \quad \text{①} \\ \text{imag.} &\rightarrow r_1 + r_2 \sin\theta_2 = r_3 \sin\theta_3 \quad \text{②} \end{aligned}$$

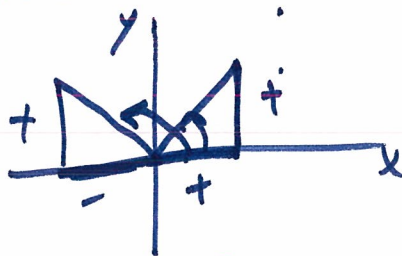
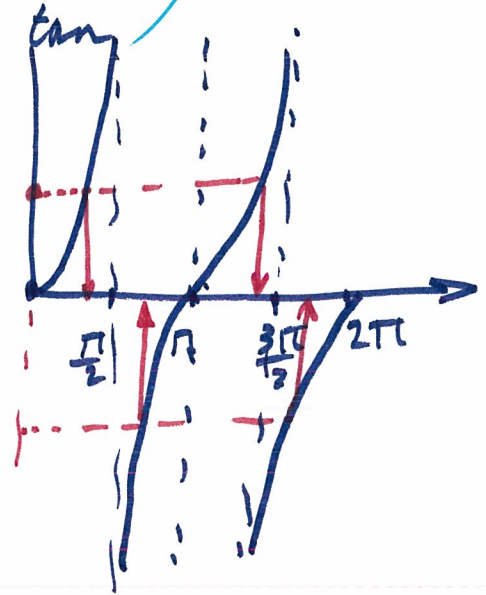
⑦ Divide ② by ① to eliminate r_3

$$\frac{r_3 \sin\theta_3}{r_3 \cos\theta_3} = \frac{r_1 + r_2 \sin\theta_2}{r_2 \cos\theta_2}$$

$$\tan\theta_3 = \frac{r_1 + r_2 \sin\theta_2}{r_2 \cos\theta_2}$$

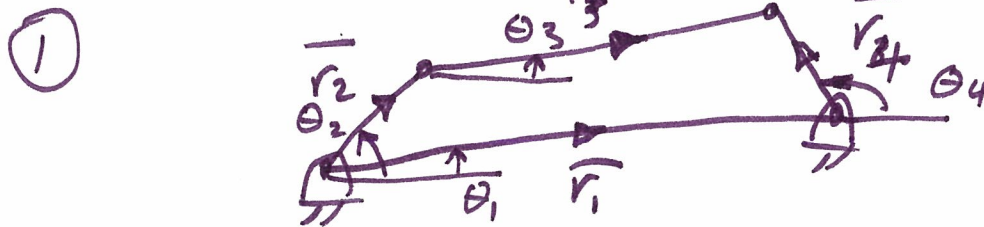
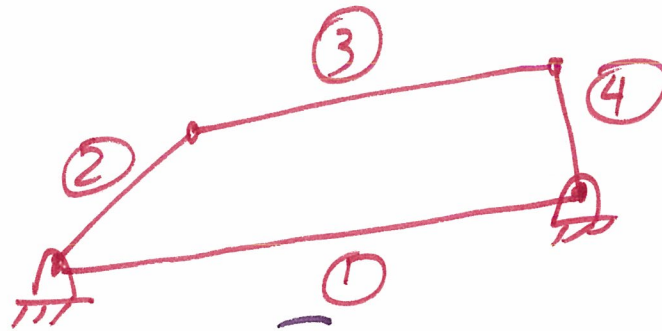
$$\theta_3 = \tan^{-1}\left(\frac{r_1 + r_2 \sin\theta_2}{r_2 \cos\theta_2}\right) \rightarrow \text{unique answer}$$

If both sides of the fraction are defined, $\tan^{-1}$ will yield a unique solution



$$\text{①} \rightarrow r_3 = \frac{r_2 \cos\theta_2}{\cos\theta_3}$$

Displacement Analysis of a 4-Bar Mechanism



$$\textcircled{2} \quad \vec{r}_2 + \vec{r}_3 = \vec{r}_1 + \vec{r}_4$$

$$\textcircled{3} \quad r_2 e^{j\theta_2} + r_3 e^{j\theta_3} = r_1 e^{j\theta_1} + r_4 e^{j\theta_4}$$

$\textcircled{4}$ input: θ_2
output: θ_3 θ_4

$$\textcircled{5} \quad r_2 (\cos \theta_2 + j \sin \theta_2) + r_3 (\cos \theta_3 + j \sin \theta_3) = r_1 (\cos \theta_1 + j \sin \theta_1) + r_4 (\cos \theta_4 + j \sin \theta_4)$$

$$\textcircled{6} \quad \begin{aligned} \text{real} &\rightarrow r_2 \cos \theta_2 + r_3 \cos \theta_3 = r_1 \cos \theta_1 + r_4 \cos \theta_4 \quad (1) \\ \text{imag.} &\rightarrow r_2 \sin \theta_2 + r_3 \sin \theta_3 = r_1 \sin \theta_1 + r_4 \sin \theta_4 \quad (2) \end{aligned}$$

⑦ Eliminate θ_3

$$r_3 \cos \theta_3 = r_1 \cos \theta_1 + r_4 \cos \theta_4 - r_2 \cos \theta_2$$

$$r_3 \sin \theta_3 = r_1 \sin \theta_1 + r_4 \sin \theta_4 - r_2 \sin \theta_2$$

Squaring & adding

$$\boxed{\sin^2 \theta + \cos^2 \theta = 1}$$

$$r_3 \cos \theta_3 = A + r_4 \cos \theta_4$$

$$r_3 \sin \theta_3 = B + r_4 \sin \theta_4$$

$$\text{where } A = r_1 \cos \theta_1 - r_2 \cos \theta_2$$

$$B = r_1 \sin \theta_1 - r_2 \sin \theta_2$$

non θ_4 terms

$$r_3^2 \cos^2 \theta_3 + r_3^2 \sin^2 \theta_3$$

$$= (A + r_4 \cos \theta_4)^2 + (B + r_4 \sin \theta_4)^2$$

$$r_3^2 = A^2 + 2Ar_4 \cos \theta_4 + \boxed{r_4^2 \cos^2 \theta_4} + B^2 + 2Br_4 \sin \theta_4 + \boxed{r_4^2 \sin^2 \theta_4}$$

$$r_3^2 = A^2 + 2Ar_4 \cos \theta_4 + B^2 + 2Br_4 \sin \theta_4 + r_4^2$$

Rearranging

$$2Ar_4 \cos \theta_4 + 2Br_4 \sin \theta_4 = r_3^2 - A^2 - B^2 - r_4^2 \quad (3)$$

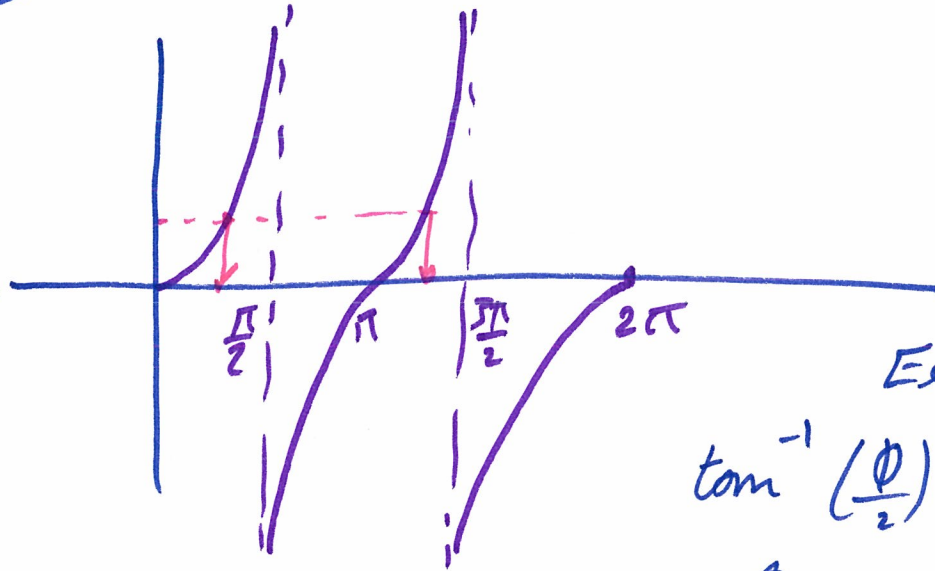
→ 1 equation

1 unknown: θ_4

→ Half-Tangent Rule to solve equation in the form of:

$$a \cos \phi + b \sin \phi = c$$

Why do we use half tangent?



Example

$$\tan^{-1}\left(\frac{\phi}{2}\right) = 1$$

$$\frac{\phi}{2} = 45^\circ \text{ or } 225^\circ$$

$$\phi = 90^\circ \text{ or } 450^\circ$$

$$\downarrow$$
$$360 + 90^\circ$$

unique solution

Because $\tan^{-1}\left(\frac{\phi}{2}\right)$ are 180° apart,

ϕ are 360° "

same angle

Solve ③ base on the Half-tangent rule

↳ obtain 2 values of θ_4 :

θ_{4a} & $\theta_{4b} \rightarrow 2$ closures



Eliminate θ_4

$$r_4 \cos \theta_4 = r_2 \cos \theta_2 + r_3 \cos \theta_3 - r_1 \cos \theta_1$$

$$r_4 \sin \theta_4 = r_2 \sin \theta_2 + r_3 \sin \theta_3 - r_1 \sin \theta_1$$

$$r_4 \cos \theta_4 = C + r_3 \cos \theta_3$$

$$r_4 \sin \theta_4 = D + r_3 \sin \theta_3$$

$$\left\{ \begin{array}{l} \text{where } C = r_2 \cos \theta_2 - r_1 \cos \theta_1 \\ D = r_2 \sin \theta_2 - r_1 \sin \theta_1 \end{array} \right.$$

Squaring & adding

$$r_4^2 \cos^2 \theta_4 = (C + r_3 \cos \theta_3)^2$$

$$r_4^2 \sin^2 \theta_4 = (D + r_3 \sin \theta_3)^2$$

$$r_4^2 = C^2 + 2r_3 C \cos \theta_3 + r_3^2 \cos^2 \theta_3 + D^2 + 2r_3 D \sin \theta_3 + r_3^2 \sin^2 \theta_3$$

Rearranging

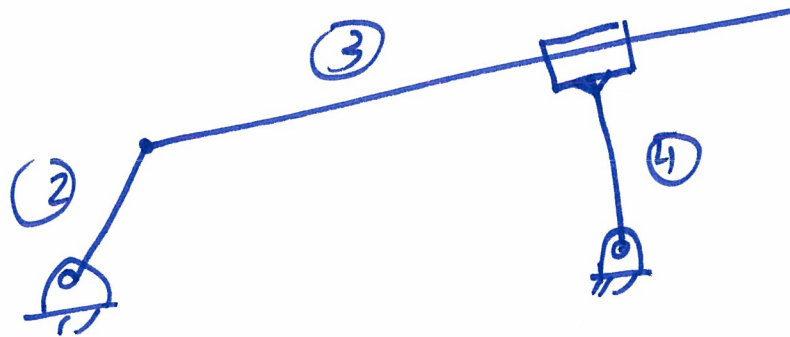
$$2r_3 C \cos \theta_3 + 2r_3 D \sin \theta_3 = r_4^2 - C^2 - D^2 - r_3^2$$

↳ solve using Half-tangent rule

θ_{3a} θ_{3b}

Example

Perform steps ① through ⑥ of displacement analysis



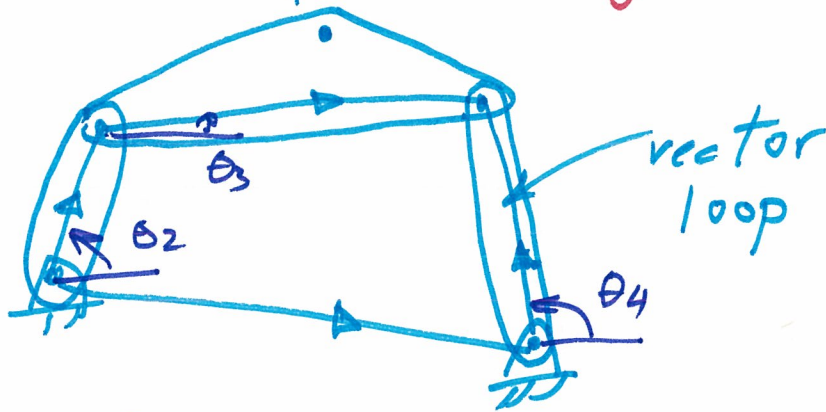
(f)W

4.18

□

figure (f)

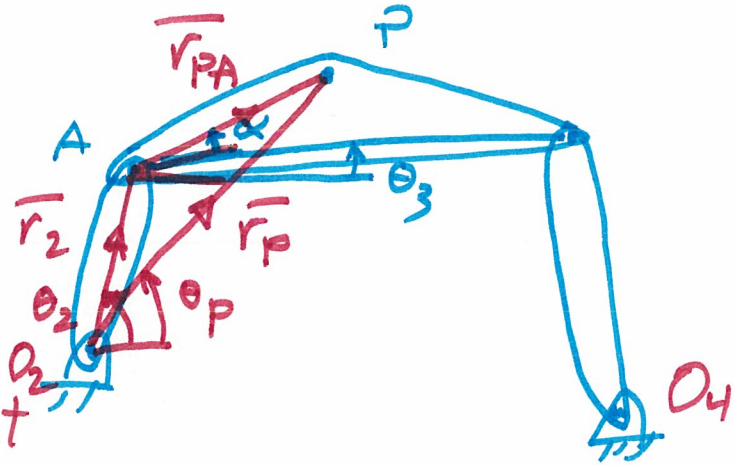
Position Analysis of a Point that Is not a Joint



- * To analyze the position (displacement) of P , a secondary analysis is needed.
- * The first step is to analyze position of the machine using vector loop & complex phasors approach $\rightarrow$ In this example, find θ_3 & θ_4 in terms of input (θ_2)

* Create a vector loop describing point P

* $\vec{r}_{PA}$ describes the relative position of P with respect to A



* α is the angle between $\vec{r}_3$ & $\vec{r}_{PA}$ (Fixed)

$$\textcircled{1} \quad \vec{r}_2 + \vec{r}_{PA} = \vec{r}_P$$

$$\textcircled{2} \quad r_2 e^{j\theta_2} + r_{PA} e^{j(\theta_3 + \alpha)} = r_P e^{j\theta_P}$$

$$\textcircled{3} \quad \begin{array}{l} \text{input: } \theta_2 \quad \theta_3 \\ \text{output: } \theta_P \quad r_P \end{array}$$

$$\textcircled{4} \quad r_2 (\cos \theta_2 + j \sin \theta_2) + r_{PA} (\cos(\theta_3 + \alpha) + j \sin(\theta_3 + \alpha)) = r_P (\cos \theta_P + j \sin \theta_P)$$

$$\textcircled{5} \quad \begin{array}{ll} \text{real} \rightarrow r_2 \cos \theta_2 + r_{PA} \cos(\theta_3 + \alpha) = r_P \cos \theta_P & \textcircled{1} \\ \text{imag.} \rightarrow r_2 \sin \theta_2 + r_{PA} \sin(\theta_3 + \alpha) = r_P \sin \theta_P & \textcircled{2} \end{array}$$

Squaring & adding

$$(r_2 \cos \theta_2 + r_{PA} \cos(\theta_3 + \alpha))^2 + (r_2 \sin \theta_2 + r_{PA} \sin(\theta_3 + \alpha))^2$$

$$= r_p^2 \cos^2 \theta_p + r_p^2 \sin^2 \theta_p$$

exploiting $\sin^2 + \cos^2 = 1$ identity

$$r_2^2 + r_{PA}^2 + 2 r_2 r_{PA} \cos \theta_2 \cos(\theta_3 + \alpha) + 2 r_2 r_{PA} \sin \theta_2 \sin(\theta_3 + \alpha) = r_p^2$$

identity $\cos a \cos b + \sin a \sin b = \cos(a-b)$

$$r_2^2 + r_{PA}^2 + 2 r_2 r_{PA} \cos(\theta_3 + \alpha - \theta_2) = r_p^2$$

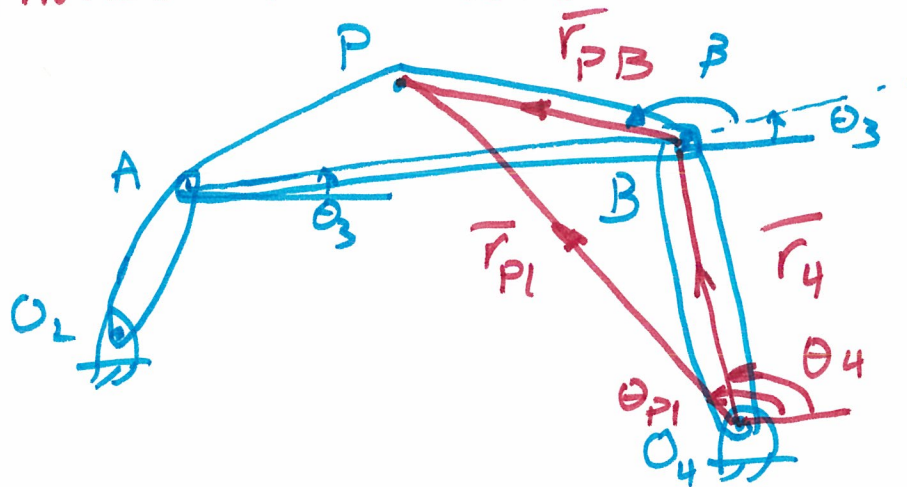
$$r_p = [r_2^2 + r_{PA}^2 + 2 r_2 r_{PA} \cos(\theta_3 + \alpha - \theta_2)]^{1/2}$$

Dividing ② by ①

$$\tan \theta_p = \frac{(r_2 \sin \theta_2 + r_{PA} \sin(\theta_3 + \alpha))}{(r_2 \cos \theta_2 + r_{PA} \cos(\theta_3 + \alpha))}$$

use the signs of the two sides of the fraction to obtain a unique solution

Alternative Formulation



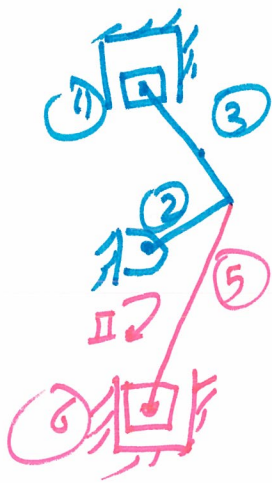
$$\vec{r}_4 + \vec{r}_{PB} = \vec{r}_{PI}$$

$$r_4 e^{j\theta_4} + r_{PB} e^{j(\theta_3 + \beta)} = r_{PI} e^{j\theta_{PI}}$$

Position Analysis of Machines with Multiple Loops

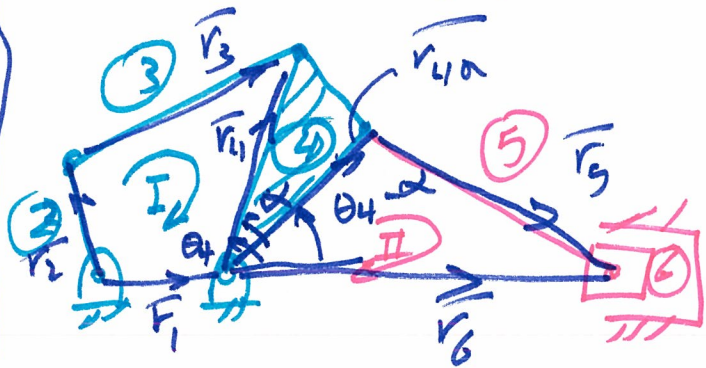
Loops

Parallel



* Loops can be solved separately

Series



* Loops have to be solved in the same sequence motion is transmitted

* In the example above

Loop I

input: θ_2

output: θ_3, θ_4

Loop II: ~~II~~

input: θ_4

output: r_6, θ_5

HW 4.19 4.22 Due Tuesday
Computer Simulation