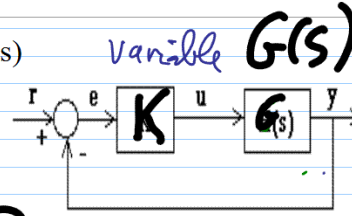


Chapter 5 Root Locus

Note Title

10/7/2011

The root locus of an (open-loop) transfer function $G(s)$ is a plot of the locations (locus) of all possible closed loop poles with proportional gain k and unity feedback:



The closed-loop transfer function is:

$$0 < K < \infty$$

and thus the poles of the closed loop system are values

$$\frac{Y(s)}{R(s)} = \frac{KG(s)}{1 + KG(s)}$$

RLocus is plot of all roots of the CLOSED LOOP char. eq. for $0 < K < \infty$

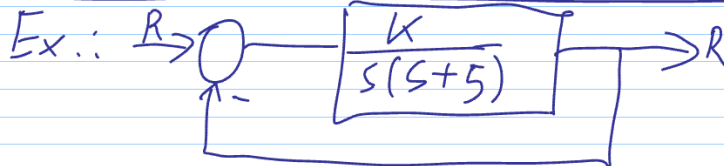
for $K=0$ RL starts in open-loop poles

$$K$$

and terminates in ∞ or in open-loop zeros.

$$s(0.5s+1)(s+1)$$

$$0 \quad -2 \quad -1$$

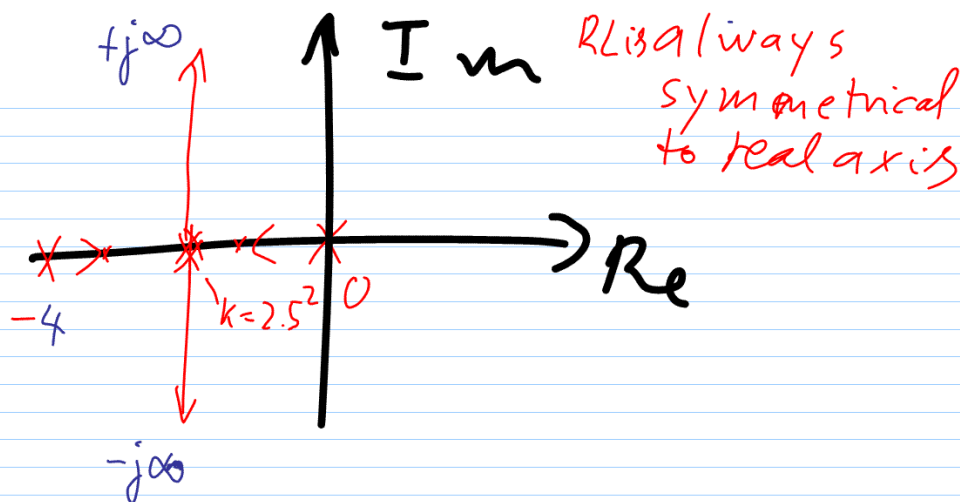


$$\frac{Y}{R} = \frac{K}{s(s+5) + K} = 0 \quad s^2 + 5s + K = 0$$

$$2.5^2 = 6.25 \quad p_{1,2} = -\frac{5}{2} \pm \sqrt{\left(\frac{5}{2}\right)^2 - K}$$

$$\text{for } k > 6.25: \text{Re}(p_i) = -2.5$$

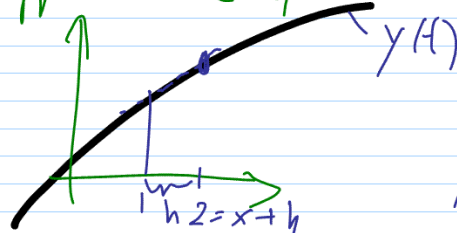
$$K \rightarrow \infty \quad \text{Im}(p_i) \Rightarrow \pm j \infty$$



Controller output $U(s) = \frac{k(s+z_1)(s+z_2)}{(s+p_1)(s+p_2)} \cdot E(s)$

$$a\ddot{u} + b\dot{u} + c \cdot u = \alpha \ddot{e} + \beta \dot{e} + \gamma \cdot e(t)$$

Difference equation



$$\dot{y} = f(x)$$

start at 1

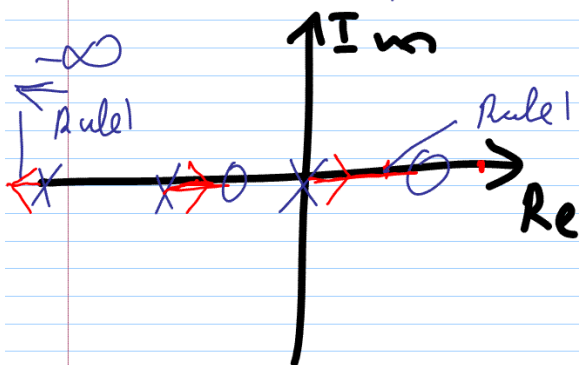
$$y_2 = y_1 + h \cdot \left. \frac{dy}{dt} \right|_1$$

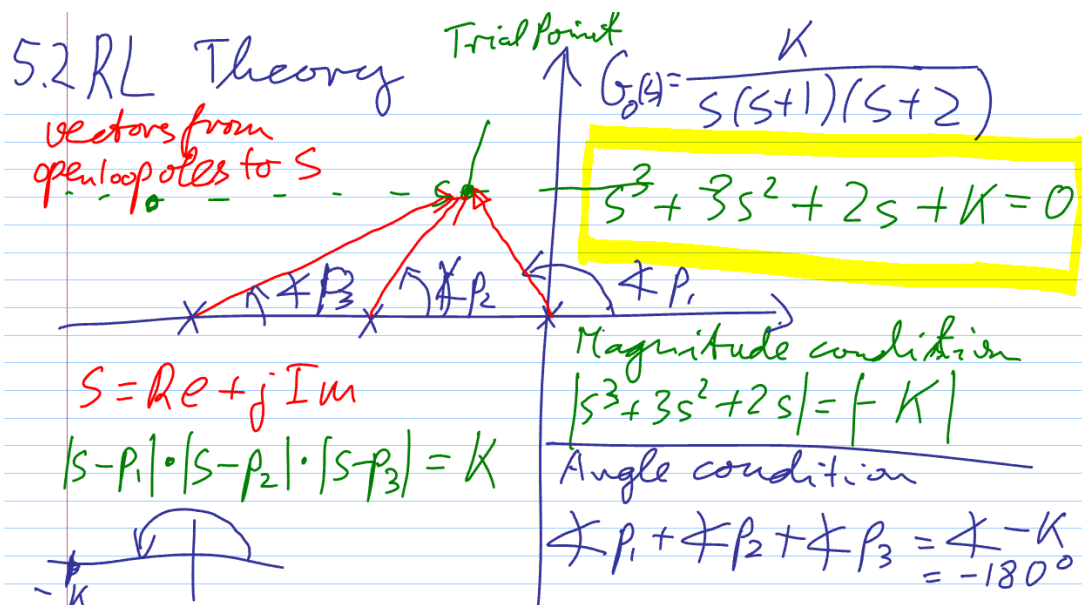
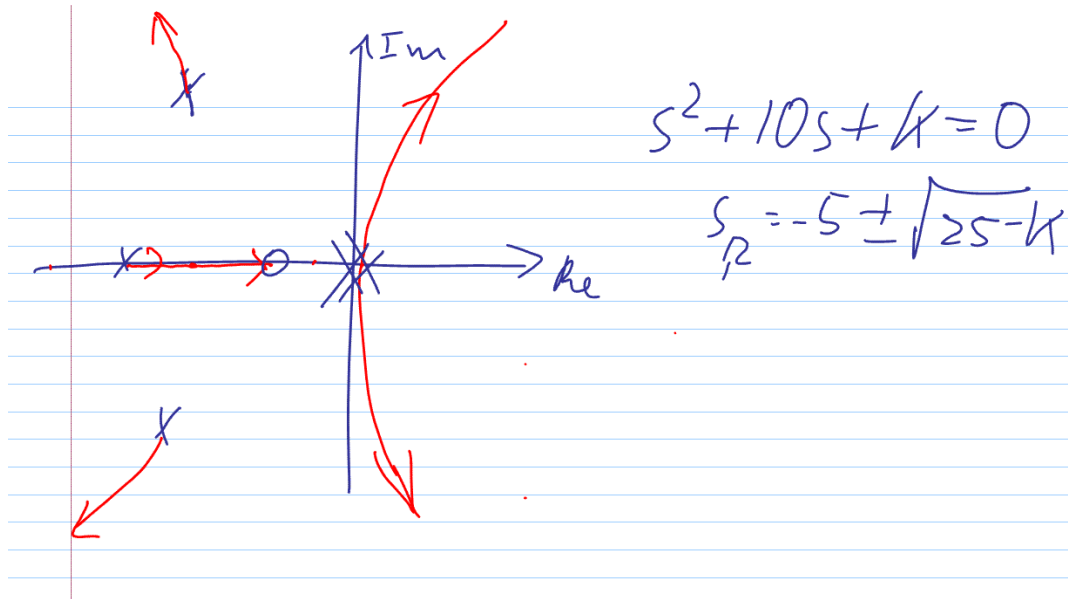
Details see ch. 8

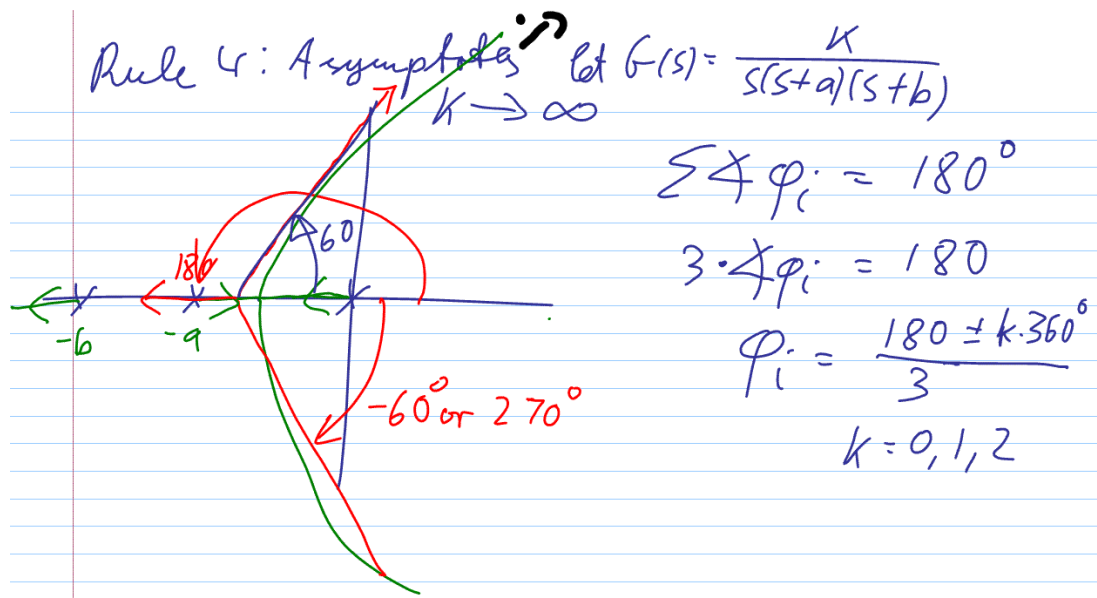
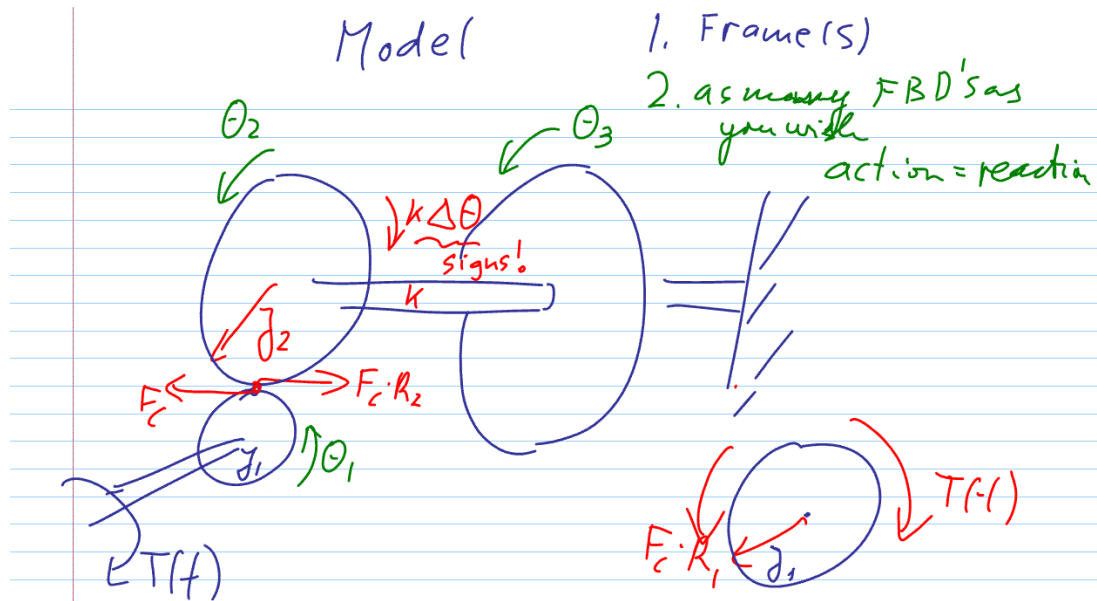
Digital Control

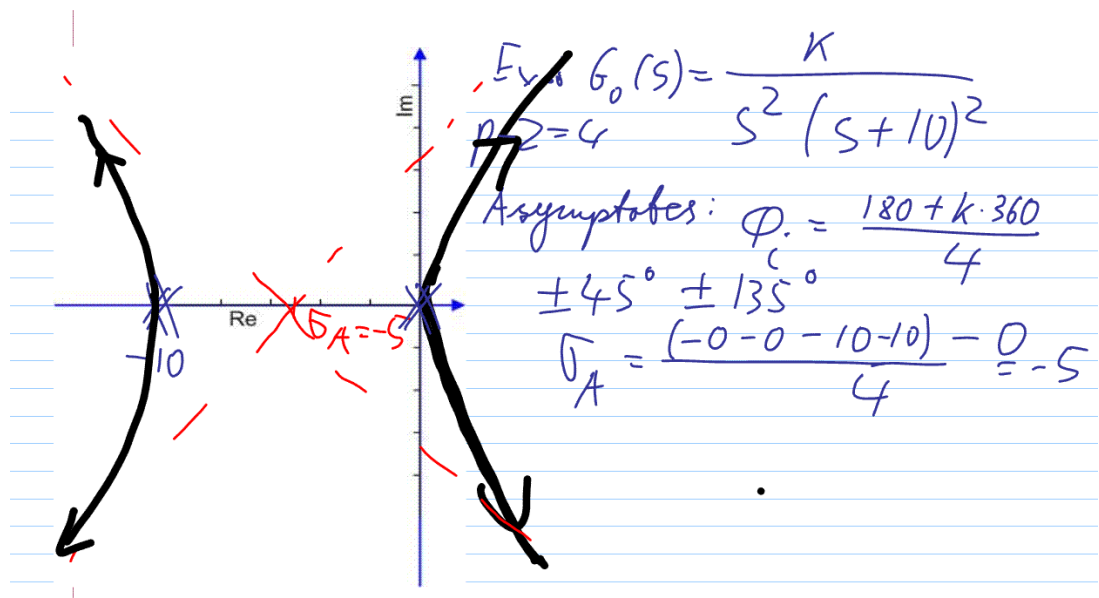
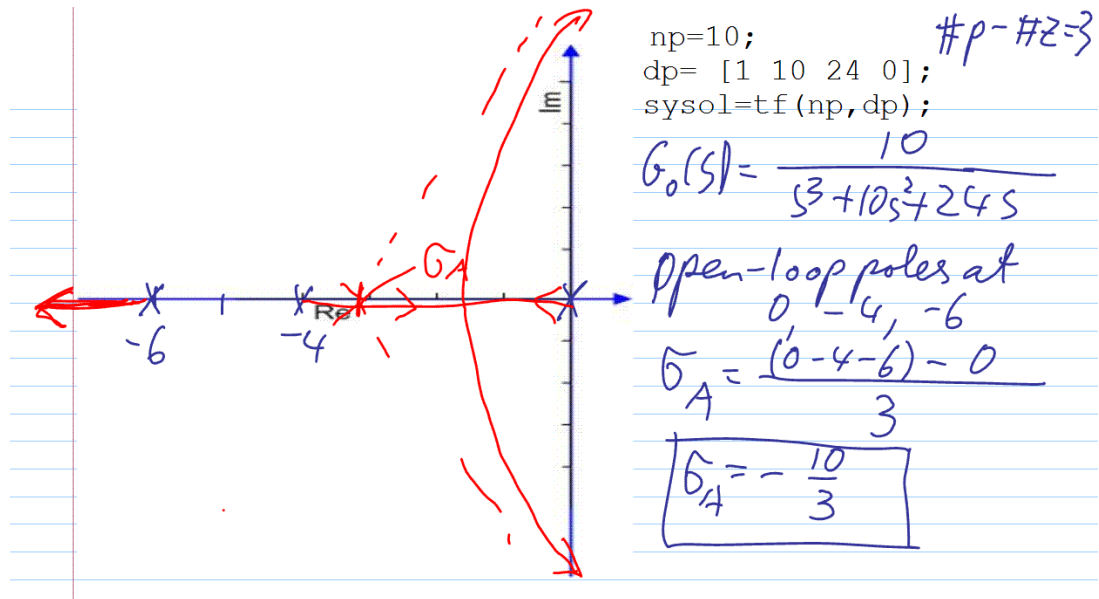
RL on Real Axis

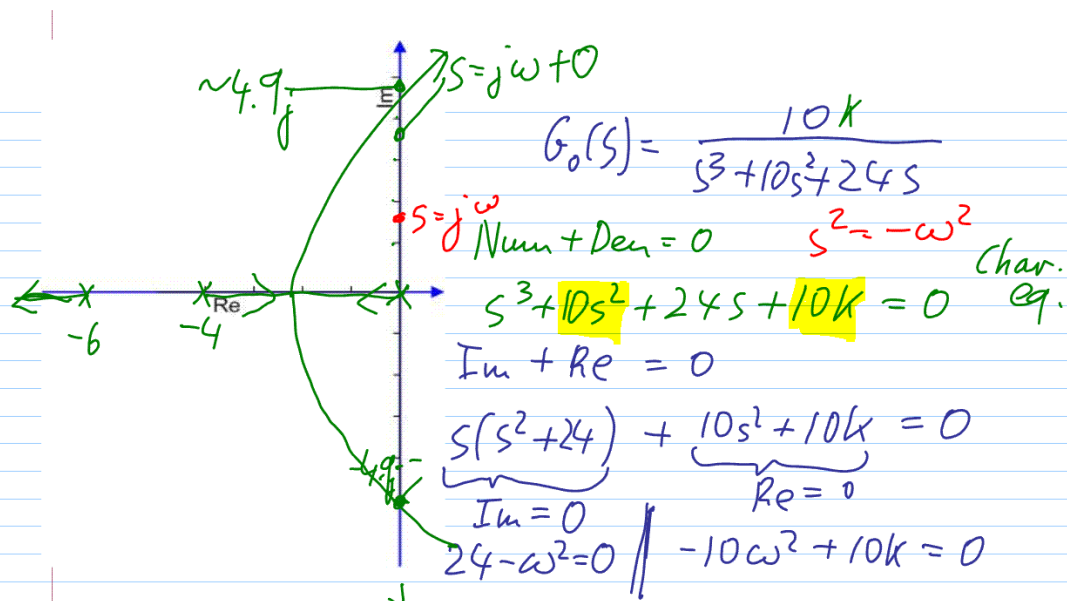
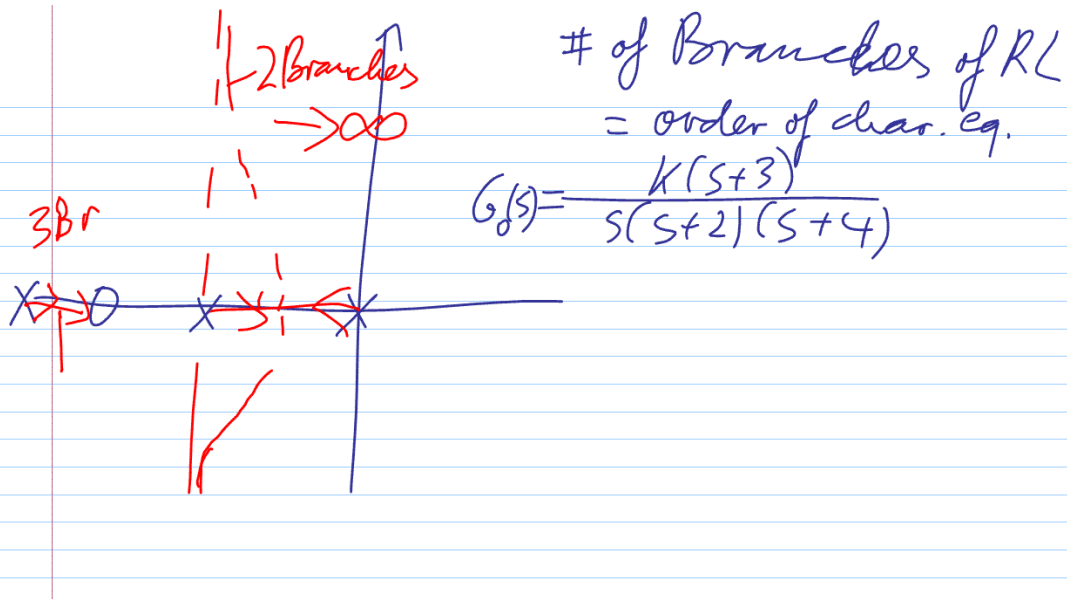
Rule 1:











Group polynomial: odd $\rightarrow \text{Im}(s) = 0$
 even $\text{Re}(s) = 0$

$$\omega^2 = 24 \Rightarrow \omega = \pm \sqrt{24} \cdot j$$

insert into $\text{Re} = 0$: $-10 \cdot 24 + 10K = 0$

$$K_{\text{crit}} = 24$$

Project

Time management

Estimation of Effort required

Modeling: ME 330

why? project is open-ended

prep. for reality

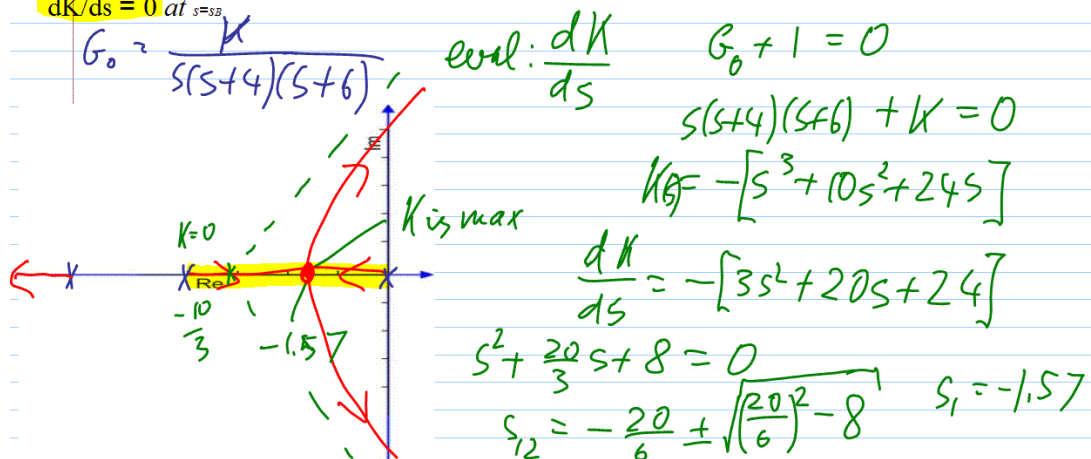
Steady state gain (ch. 3)

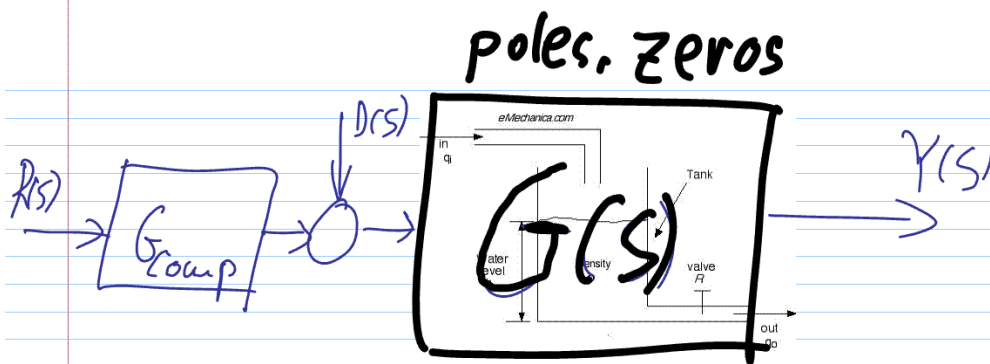
The steady state gain of a system is the ratio **output/input** in the steady state. The steady state gain is $Y_{ss}/R_{ss} = G(s=0)$
 Caution: Disregard Integrators!

$$\frac{Y}{R} = \frac{K(s+z_1)\dots}{(s+p_1)(s+p_2)\dots} \quad K_{ss} = \frac{Kz_1\dots}{p_1 p_2 \dots}$$

Rule #5 (Breakaway Points): For $K > 0$, the root locus breaks away from the **real axis** at points of relative maximum K and re-enters the real axis at points of relative minimum K . i.e., breakaway and re-entry occur at points s_B where

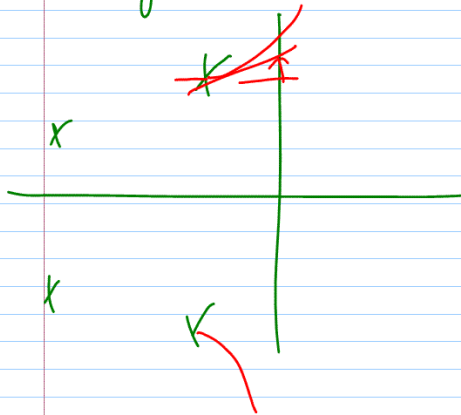
$$dK/ds = 0 \text{ at } s=s_B$$



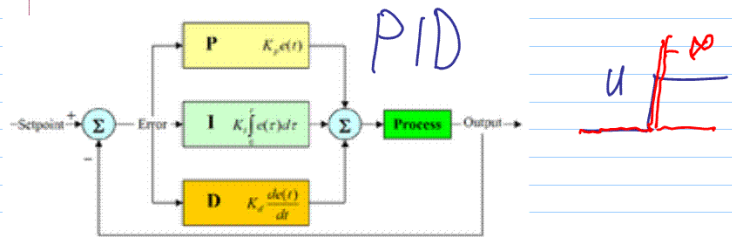


want $Y(s) = 1 \cdot R(s)$ we get $G_p^{-1} \cdot G_p = 1$

Angles of Departure (read!)



5.4 Root Locus Design : Compensators



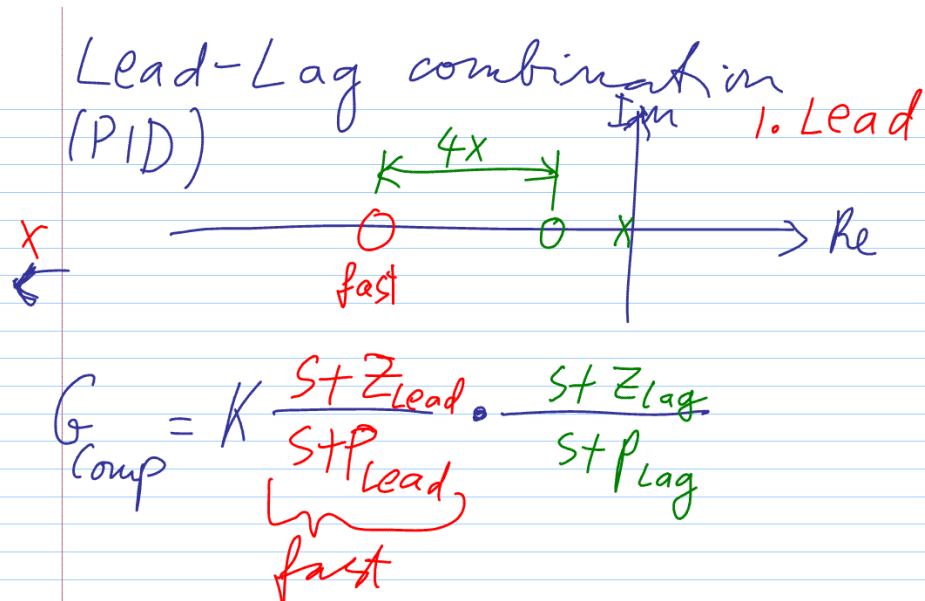
$$u(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau + K_d \frac{d}{dt} e(t)$$

$$\frac{U}{E} = K_p + \frac{K_i}{s} + K_d s = \frac{K_p \cdot s + K_i + K_d s^2}{s}$$

$$= \frac{(T_a s + 1)(T_B s + 1)}{s} \text{ Differentiator}$$

PD-controller
more realistic
 Lead = $\frac{s+z}{s+p}$ $|z| < |p|$

PI Lag = $\frac{s+z}{s+p}$ $|z| > |p|$
slow
 $|p| \approx 0$

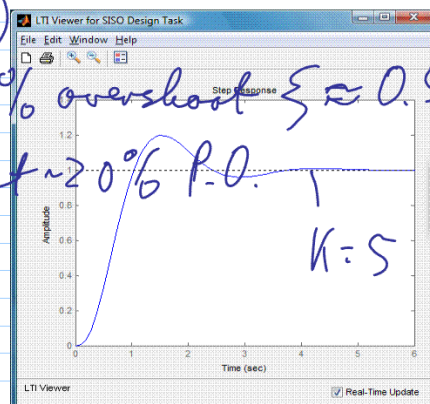


Lead Design Example

Plant $G(s) = \frac{K}{s(s+4)(s+6)}$

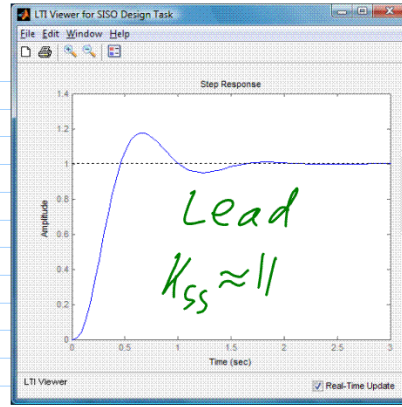
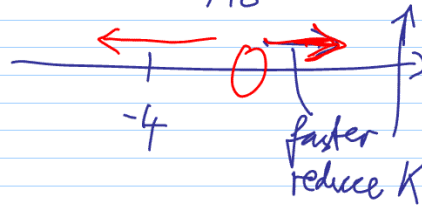
P-control, design for 20% overshoot $\xi \approx 0.5$

vary K for $K=5$ we get $\approx 20\%$ P.O.



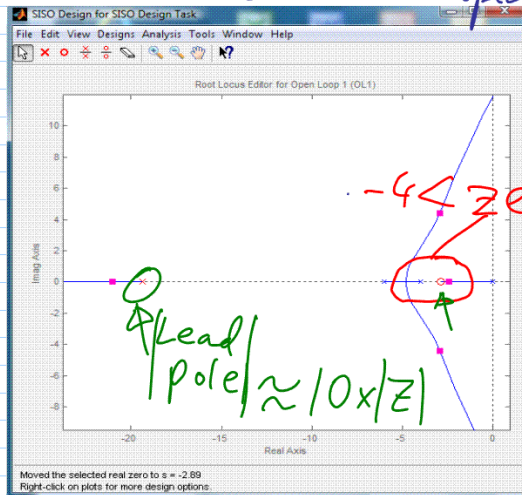
Lead

$$G_{lead} \approx 11 \frac{s/3 + 1}{s/18 + 1}$$



$$\frac{s+3}{s+18} \cdot \frac{18}{3}$$

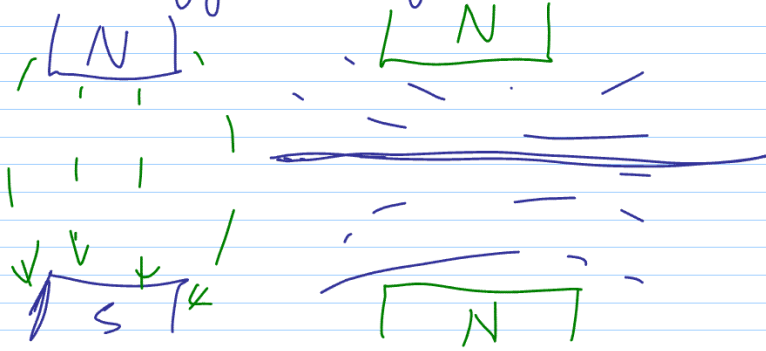
Wed.: Review Topics ch. 3.5... 5



Poles and zeros

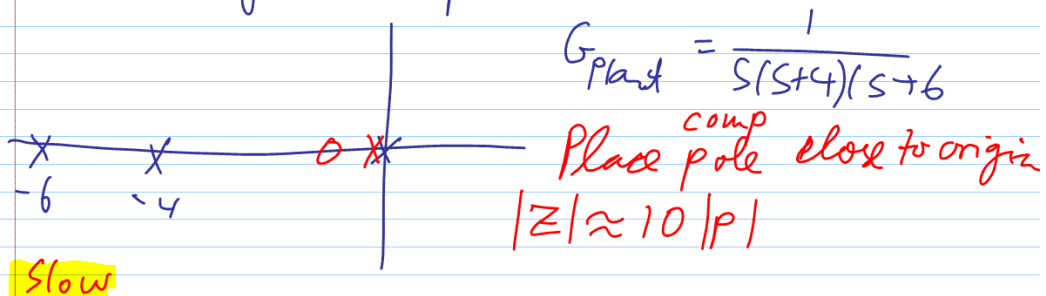
X → ← X o
repel attractor

analogy to magnetic fields



$$\text{Lead } G_{\text{lead}} = \frac{s+z}{s+p} \approx PD |P| \gg |z|$$

$$\text{Lag } G_{\text{lag}} = \frac{s+z}{s+p} \approx PI |z| \gg |p|$$

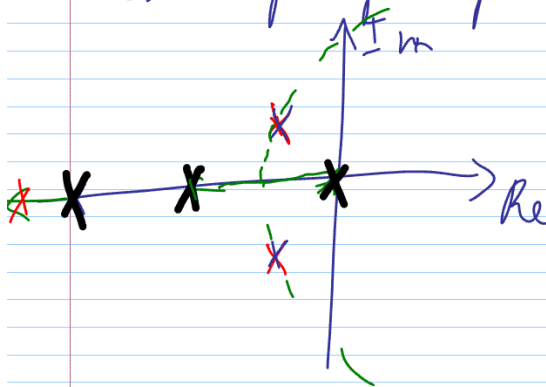


Purpose of Lag: Reduce S.S. error

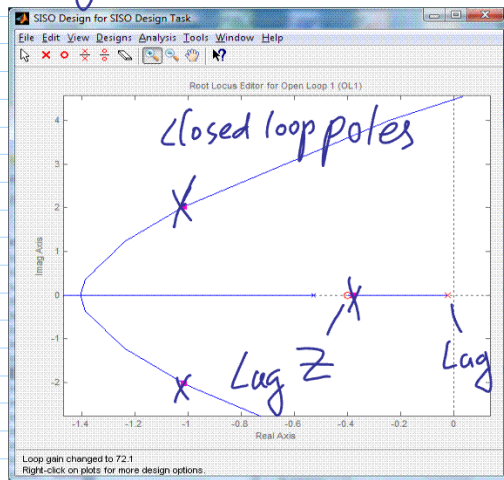
When using combined Lead-Lag

1. Design Lead (fast)
2. Add Lag

Relation of closed loop poles in R.L. with closed loop step response. See Ch. 3. 4

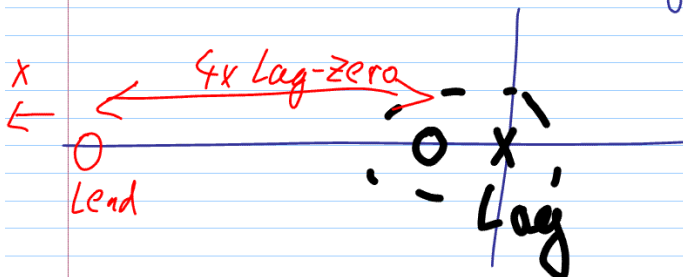


$$\text{Lag} = \frac{s+0.4}{s+0.02} \quad K_{SS} = 72 \cdot \frac{s/0.4 + 1}{s/0.02 + 1}$$



Lead-Lag controller (PID)

$$G_{comp} = \frac{s + z_{lead}}{s + p_{lead}} \cdot \frac{s + z_{lag}}{s + p_{lag}}$$



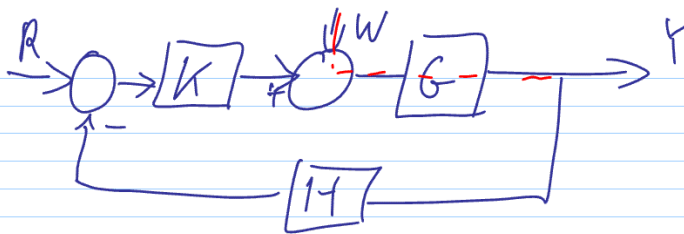
use only for $\zeta < 1$ will post Notes on web

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{9}{s^2 + 4s + 9}$$

$$\omega_n = 3$$

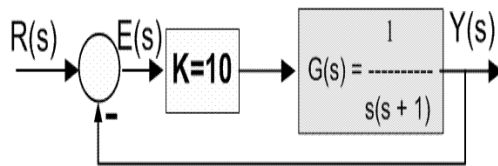
$$2\zeta\omega_n = 4 \rightarrow \zeta = \frac{4}{2 \cdot 3} = \frac{2}{3}$$

when $\zeta \geq 1 \rightarrow 2$ real poles



$$Y = G \cdot W + KG(R - H \cdot Y)$$

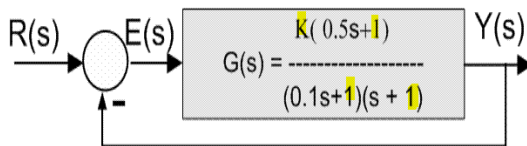
$$Y = \frac{G \cdot W}{1 + KGH} + \frac{KG \cdot R}{1 + KGH}$$



$$E_{ss} = \lim_{s \rightarrow 0} s \cdot \frac{1}{s} \cdot \frac{1}{s(s+1) + K}$$

$$E_{ss} = \frac{1}{1 + G_0} = \frac{1}{1 + \frac{10}{s(s+1)}} = \frac{1}{1 + \infty}$$

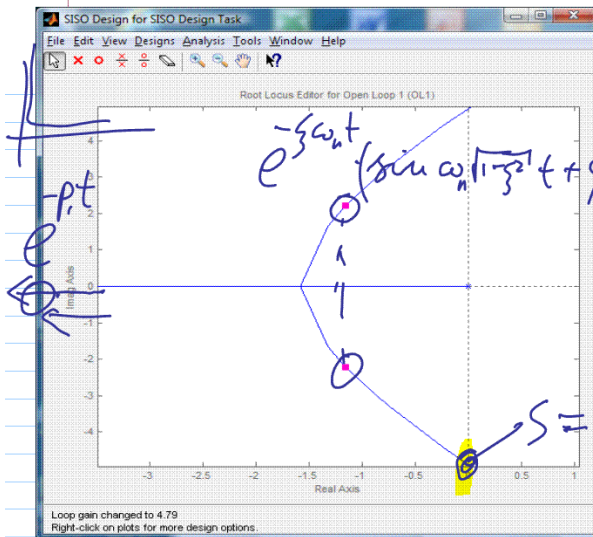
$$E_{ss} \rightarrow 0$$



Ramp

$$K_V = \lim_{s \rightarrow 0} s \cdot G_0(s) = 0$$

$$E_{ss} = \frac{1}{K_V} \Rightarrow \infty$$



$$G_0 = \frac{10}{s(s+4)(s+6)}$$

Choice $K = 4.78$
results in 3 closed
loop poles

Im. axis crossings: find K_{crit} , ω_n at
 $s = j\omega + 0 \cdot Re$

$$s^3 + 10s^2 + 24s + 10 \cdot K = 0$$

$$Im = 0: j\omega(-\omega^2 + 24) = 0 \quad \omega_n = \sqrt{24}$$

$$Re = 0: 10 \cdot (-\omega^2) + 10K = 0$$

$$10K - 240 = 0 \quad K_{crit} = 24$$

Add zero

$$G_0 = \frac{10(s+z)}{s(s+4)(s+6)}$$

$$\#A_s = 2 = \#p_i - \#z_i$$